

CPC COOPERATIVE PATENT CLASSIFICATION

H ELECTRICITY

(NOTE omitted)

H02 GENERATION; CONVERSION OR DISTRIBUTION OF ELECTRIC POWER

H02P CONTROL OR REGULATION OF ELECTRIC MOTORS, ELECTRIC GENERATORS OR DYNAMO-ELECTRIC CONVERTERS; CONTROLLING TRANSFORMERS, REACTORS OR CHOKE COILS

NOTES

1. This subclass covers arrangements for starting, regulating, electronically commutating, braking, or otherwise controlling motors, generators, dynamo-electric converters, clutches, brakes, gears, transformers, reactors or choke coils, of the types classified in the relevant subclasses, e.g. [H01F](#), [H02K](#).
2. This subclass does not cover similar arrangements for the apparatus of the types classified in subclass [H02N](#), which arrangements are covered by that subclass.
3. In this subclass, the following terms or expressions are used with the meanings indicated:
 - "control" means influencing a variable in any way, e.g. changing its direction or its value (including changing it to or from zero), maintaining it constant or limiting its range of variation;
 - "regulation" means maintaining a variable at a desired value, or within a desired range of values, by comparison of the actual value with the desired value.
4. In this subclass, it is desirable to add the indexing codes of groups [H02P 2101/00](#) and [H02P 2103/00](#)

WARNING

In this subclass non-limiting references (in the sense of paragraph 39 of the Guide to the IPC) may still be displayed in the scheme.

1/00	Arrangements for starting electric motors or dynamo-electric converters (starting of synchronous motors with electronic commutators except reluctance motors, H02P 6/20, H02P 6/22; starting dynamo-electric motors rotating step by step H02P 8/04; vector control H02P 21/00)	1/10	. . . Manually-operated on/off switch controlling relays or contactors operating sequentially for starting a motor (sequence determined by power-operated multi-position switch H02P 1/08)
		1/12	. . . Switching devices centrifugally operated by the motor
		1/14	. . . Pressure-sensitive resistors centrifugally operated by the motor
		1/16	. for starting dynamo-electric motors or dynamo-electric converters
		1/163	. . {for starting an individual reluctance motor}
		1/166	. . {Driving load with high inertia}
		1/18	. . for starting an individual dc motor
		1/20	. . . by progressive reduction of resistance in series with armature winding
		1/22	. . . in either direction of rotation
		1/24	. . for starting an individual ac commutator motor (starting of ac/dc commutator motors H02P 1/18)
		1/26	. . for starting an individual polyphase induction motor
		1/265	. . . {Means for starting or running a triphase motor on a single phase supply}
		1/28	. . . by progressive increase of voltage applied to primary circuit of motor
		1/30	. . . by progressive increase of frequency of supply to primary circuit of motor
		1/32	. . . by star-delta switching
		1/34	. . . by progressive reduction of impedance in secondary circuit
		1/36 the impedance being a liquid resistance
		1/38	. . . by pole-changing
1/02	. Details		
1/021	. . {Protection against "no voltage condition"}		
1/022	. . {Security devices, e.g. correct phase sequencing}		
1/023	. . . {Protection against sparking of contacts or sticking together}		
1/024	. . . {Protection against simultaneous starting by two starting devices}		
1/025	. . . {Protection against starting if starting resistor is not at zero position}		
1/026	. . . {Means for delayed starting}		
1/027	. . {Special design of starting resistor}		
1/028	. . {wherein the motor voltage is increased at low speed, to start or restart high inertia loads}		
1/029	. . {Restarting, e.g. after power failure}		
1/04	. . Means for controlling progress of starting sequence in dependence upon time or upon current, speed, or other motor parameter		
1/06	. . . Manually-operated multi-position starters		
1/08	. . . Manually-operated on/off switch controlling power-operated multi-position switch or impedances for starting a motor		

- 1/40 . . . in either direction of rotation
- 1/42 . . for starting an individual single-phase induction motor { (H02P 27/04 takes precedence) }
- 1/423 . . . {by using means to limit the current in the main winding}
- 1/426 . . . {by using a specially adapted frequency converter}
- 1/44 . . . by phase-splitting with a capacitor
- 1/445 {by using additional capacitors switched at start up}
- 1/46 . . for starting an individual synchronous motor { (H02P 27/04 takes precedence) }
- 1/465 . . . {for starting an individual single-phase synchronous motor}
- 1/48 . . . by pole-changing
- 1/50 . . . by changing over from asynchronous to synchronous operation (H02P 1/48 takes precedence)
- 1/52 . . . by progressive increase of frequency of supply to motor
- 1/54 . . for starting two or more dynamo-electric motors
- 1/56 . . . simultaneously
- 1/58 . . . sequentially
- 3/00 Arrangements for stopping or slowing electric motors, generators, or dynamo-electric converters (stopping of synchronous motors with electronic commutators except reluctance motors, H02P 6/24; stopping dynamo-electric motors rotating step by step H02P 8/24; vector control H02P 21/00)**
- 3/02 . Details
- 3/025 . . {holding the rotor in a fixed position after deceleration}
- 3/04 . . Means for stopping or slowing by a separate brake, e.g. friction brake, eddy-current brake (brakes F16D, H02K 49/00)
- 3/06 . for stopping or slowing an individual dynamo-electric motor or dynamo-electric converter
- 3/065 . . {for stopping or slowing a reluctance motor}
- 3/08 . . for stopping or slowing a dc motor
- 3/10 . . . by reversal of supply connections
- 3/12 . . . by short-circuit or resistive braking
- 3/14 . . . by regenerative braking
- 3/16 . . . by combined electrical and mechanical braking
- 3/18 . . for stopping or slowing an ac motor
- 3/20 . . . by reversal of phase sequence of connections to the motor
- 3/22 . . . by short-circuit or resistive braking
- 3/24 . . . by applying dc to the motor
- 3/26 . . . by combined electrical and mechanical braking
- 4/00 Arrangements specially adapted for regulating or controlling the speed or torque of electric motors that can be connected to two or more different electric power supplies (vector control H02P 21/00)**
- 5/00 Arrangements specially adapted for regulating or controlling the speed or torque of two or more electric motors (H02P 6/04, H02P 8/40 take precedence)**
- 5/46 . for speed regulation of two or more dynamo-electric motors in relation to one another
- 5/48 . . by comparing mechanical values representing the speeds
- 5/485 . . . using differential movement of the two motors, e.g. using differential gearboxes
- 5/49 . . . by intermittently closing or opening electrical contacts
- 5/50 . . by comparing electrical values representing the speeds
- 5/505 . . . using equalising lines, e.g. rotor and stator lines of first and second motors
- 5/51 . . . Direct ratio control
- 5/52 . . additionally providing control of relative angular displacement
- 5/54 . . . Speed and position comparison between the motors by mechanical means
- 5/56 . . . Speed and position comparison between the motors by electrical means
- 5/60 . controlling combinations of dc and ac dynamo-electric motors (H02P 5/46 takes precedence)
- 5/68 . controlling two or more dc dynamo-electric motors (H02P 5/46, H02P 5/60 take precedence)
- 5/685 . . electrically connected in series, i.e. carrying the same current
- 5/69 . . mechanically coupled by gearing
- 5/695 . . . Differential gearing
- 5/74 . controlling two or more ac dynamo-electric motors (H02P 5/46, H02P 5/60 take precedence)
- 5/747 . . mechanically coupled by gearing
- 5/753 . . . Differential gearing
- 6/00 Arrangements for controlling synchronous motors or other dynamo-electric motors using electronic commutation dependent on the rotor position; Electronic commutators therefor (vector control H02P 21/00)**
- NOTE**
- Group H02P 6/26 takes precedence over groups H02P 6/04–H02P 6/24 and H02P 6/28 – H02P 6/34
- 6/005 . {Arrangements for controlling doubly fed motors}
- 6/006 . {Controlling linear motors}
- 6/007 . {wherein the position is detected using the ripple of the current caused by the commutation}
- 6/04 . Arrangements for controlling or regulating the speed or torque of more than one motor (H02P 6/10 takes precedence)
- 2006/045 . . {Control of current}
- 6/06 . Arrangements for speed regulation of a single motor wherein the motor speed is measured and compared with a given physical value so as to adjust the motor speed
- 6/08 . Arrangements for controlling the speed or torque of a single motor (H02P 6/10, H02P 6/28 take precedence)
- 6/085 . . {in a bridge configuration}
- 6/10 . Arrangements for controlling torque ripple, e.g. providing reduced torque ripple
- 6/12 . Monitoring commutation; Providing indication of commutation failure
- 6/14 . Electronic commutators
- 6/15 . . Controlling commutation time
- 6/153 . . . {wherein the commutation is advanced from position signals phase in function of the speed}
- 6/157 . . . {wherein the commutation is function of electro-magnetic force [EMF]}

6/16 Circuit arrangements for detecting position	7/26 using discharge tubes
6/17 and for generating speed information	7/265 {whereby the speed is regulated by measuring the motor speed and comparing it with a given physical value}
6/18 without separate position detecting elements	7/28 using semiconductor devices
6/181 {using different methods depending on the speed}	7/2805 {whereby the speed is regulated by measuring the motor speed and comparing it with a given physical value}
6/182 using back-emf in windings	7/281 the DC motor being operated in four quadrants
6/183 {using an injected high frequency signal}		
6/185 using inductance sensing, e.g. pulse excitation		
6/186 {using difference of inductance or reluctance between the phases}		
6/187 {using the star point voltage}		
6/188 {using the voltage difference between the windings (H02P 6/182 takes precedence)}		
6/20 Arrangements for starting (H02P 6/08 takes precedence)	7/2815 {whereby the speed is regulated by measuring the motor speed and comparing it with a given physical value}
6/21 Open loop start	7/282 controlling field supply only
6/22 in a selected direction of rotation	7/2825 {whereby the speed is regulated by measuring the motor speed and comparing it with a given physical value}
6/24 Arrangements for stopping	7/285 controlling armature supply only
6/26 Arrangements for controlling single phase motors	7/2855 {whereby the speed is regulated by measuring the motor speed and comparing it with a given physical value}
6/28 Arrangements for controlling current (H02P 6/10 takes precedence)	7/288 using variable impedance
6/30 Arrangements for controlling the direction of rotation (H02P 6/22 takes precedence)	7/2885 {whereby the speed is regulated by measuring the motor speed and comparing it with a given physical value}
6/32 Arrangements for controlling wound field motors, e.g. motors with exciter coils	7/29 using pulse modulation
6/34 Modelling or simulation for control purposes	7/291 with on-off control between two set points, e.g. controlling by hysteresis
7/00	Arrangements for regulating or controlling the speed or torque of electric DC motors	7/2913 {whereby the speed is regulated by measuring the motor speed and comparing it with a given physical value}
7/0094 {wherein the position is detected using the ripple of the current caused by the commutator}	7/292 using static converters, e.g. AC to DC
7/02 the DC motors being of the linear type	7/293 using phase control (H02P 7/295 takes precedence)
7/025 the DC motors being of the moving coil type, e.g. voice coil motors	7/295 of the kind having a thyristor or the like in series with the power supply and the motor
7/03 for controlling the direction of rotation of DC motors	7/298 controlling armature and field supply
7/04 {by means of a H-bridge circuit}	7/2985 {whereby the speed is regulated by measuring the motor speed and comparing it with a given physical value}
7/05 {by means of electronic switching}	7/30 using magnetic devices with controllable degree of saturation, i.e. transductors
7/06 for regulating or controlling an individual dc dynamo-electric motor by varying field or armature current	7/305 {whereby the speed is regulated by measuring the motor speed and comparing it with a given physical value}
7/063 {using centrifugal devices, e.g. switch, resistor}	7/32 using armature-reaction-excited machines, e.g. metadyne, amplidyne, rototrol
7/066 {using a periodic interrupter, e.g. Tirrill regulator}	7/325 {whereby the speed is regulated by measuring the motor speed and comparing it with a given physical value}
7/08 by manual control without auxiliary power	7/34 using Ward-Leonard arrangements
7/10 of motor field only	7/343 in which both generator and motor fields are controlled
7/12 Switching field from series to shunt excitation or vice versa		
7/14 of voltage applied to the armature with or without control of field {Ward-Leonard}		
7/18 by master control with auxiliary power		
7/20 using multi-position switch, e.g. drum, controlling motor circuit by means of relays (H02P 7/24, H02P 7/30 take precedence)		
7/22 using multi-position switch, e.g. drum, controlling motor circuit by means of pilot-motor-operated multi-position switch or pilot-motor-operated variable resistance (H02P 7/24, H02P 7/30 take precedence)		
7/24 using discharge tubes or semiconductor devices		
7/245 {whereby the speed is regulated by measuring the motor speed and comparing it with a given physical value}		

NOTE

Group [H02P 7/281](#) takes precedence over groups [H02P 7/282](#) – [H02P 7/298](#).

7/347 in which only the generator field is controlled	9/04	. Control effected upon non-electric prime mover and dependent upon electric output value of the generator
7/348	. . . {for changing between series and parallel connections of motors}	9/06	. Control effected upon clutch or other mechanical power transmission means and dependent upon electric output value of the generator
8/00	Arrangements for controlling dynamo-electric motors of the kind having motors rotating step by step (vector control H02P 21/00)	9/08	. Control of generator circuit during starting or stopping of driving means, e.g. for initiating excitation
8/005	. {of linear motors}	9/10	. Control effected upon generator excitation circuit to reduce harmful effects of overloads or transients, e.g. sudden application of load, sudden removal of load, sudden change of load
8/02	. specially adapted for single-phase or bi-pole stepper motors, e.g. watch-motors, clock-motors	9/102	. . {for limiting effects of transients}
	NOTE	9/105	. . {for increasing the stability}
	Groups H02P 8/005 and H02P 8/02 take precedence over groups H02P 8/04 - H02P 8/42	9/107	. . {for limiting effects of overloads}
8/04	. Arrangements for starting	9/12	. . for demagnetising; for reducing effects of remanence; for preventing pole reversal
8/06	. . in selected direction of rotation	9/123	. . . {for demagnetising; for reducing effects of remanence}
8/08	. . Determining position before starting	9/126	. . . {for preventing pole reversal}
8/10	. . Shaping pulses for starting; Boosting current during starting	9/14	. by variation of field (H02P 9/08 , H02P 9/10 take precedence)
8/12	. Control or stabilisation of current	9/16	. . due to variation of ohmic resistance in field circuit, using resistances switched in or out of circuit step by step
8/14	. Arrangements for controlling speed or speed and torque (H02P 8/12 , H02P 8/22 take precedence)	9/18	. . . the switching being caused by a servomotor, measuring instrument, or relay
8/16	. . Reducing energy dissipated or supplied	9/20	. . due to variation of continuously-variable ohmic resistance
8/165	. . . {using two level supply voltage}	9/22	. . . comprising carbon pile resistance
8/18	. . Shaping of pulses, e.g. to reduce torque ripple	9/24	. . due to variation of make-to-break ratio of intermittently-operating contacts, e.g. using Tirrill regulator
8/20	. . characterised by bidirectional operation	9/26	. . using discharge tubes or semiconductor devices (H02P 9/34 takes precedence)
8/22	. Control of step size; Intermediate stepping, e.g. microstepping	9/28	. . . using discharge tubes
8/24	. Arrangements for stopping (H02P 8/32 takes precedence)	9/30	. . . using semiconductor devices
8/26	. . Memorising final pulse when stopping	9/302 {Brushless excitation}
8/28	. . Disconnecting power source when stopping	9/305 {controlling voltage (H02P 9/302 takes precedence)}
8/30	. . Holding position when stopped	9/307 {more than one voltage output}
8/32	. Reducing overshoot or oscillation, e.g. damping	9/32	. . using magnetic devices with controllable degree of saturation (H02P 9/34 takes precedence)
8/34	. Monitoring operation (H02P 8/36 takes precedence)	9/34	. . using magnetic devices with controllable degree of saturation in combination with controlled discharge tube or controlled semiconductor device
8/36	. Protection against faults, e.g. against overheating, step-out; Indicating faults (emergency protective arrangements with automatic interruption of supply H02H 7/08)	9/36	. . using armature-reaction-excited machines
8/38	. . the fault being step-out	9/38	. . Self-excitation by current derived from rectification of both output voltage and output current of generator
8/40	. Special adaptations for controlling two or more stepping motors	9/40	. by variation of reluctance of magnetic circuit of generator
8/42	. characterised by non-stepper motors being operated step by step	9/42	. to obtain desired frequency without varying speed of the generator
9/00	Arrangements for controlling electric generators for the purpose of obtaining a desired output (Ward-Leonard arrangements H02P 7/34; vector control H02P 21/00; feeding a network by two or more generators H02J; for charging batteries H02J 7/14)	9/44	. Control of frequency and voltage in predetermined relation, e.g. constant ratio
9/006	. {Means for protecting the generator by using control (H02H 7/06 takes precedence; control effected upon generator excitation circuit to reduce harmful effects of overloads or transients H02P 9/10)}	9/46	. Control of asynchronous generator by variation of capacitor
9/007	. {Control circuits for doubly fed generators}	9/48	. Arrangements for obtaining a constant output value at varying speed of the generator, e.g. on vehicle (H02P 9/04 - H02P 9/46 take precedence)
9/008	. {wherein the generator is controlled by the requirements of the prime mover}		
9/009	. {Circuit arrangements for detecting rotor position}		
9/02	. Details		

11/00	Arrangements for controlling dynamo-electric converters (starting H02P 1/00 ; stopping or slowing H02P 3/00 ; vector control H02P 21/00 ; feeding a network in conjunction with a generator or another converter H02J)	21/05	• specially adapted for damping motor oscillations, e.g. for reducing hunting
11/04	• for controlling dynamo-electric converters having a dc output	21/06	• Rotor flux based control involving the use of rotor position or rotor speed sensors
11/06	• for controlling dynamo-electric converters having an ac output	21/08	• • Indirect field-oriented control; Rotor flux feed-forward control
13/00	Arrangements for controlling transformers, reactors or choke coils, for the purpose of obtaining a desired output (regulation systems using transformers, reactors or choke coils G05F ; transformers H01F ; feeding a network in conjunction with a generator or a converter H02J ; control or regulation of converters H02M)	21/09	• • • Field phase angle calculation based on rotor voltage equation by adding slip frequency and speed proportional frequency
13/06	• by tap-changing; by rearranging interconnections of windings	21/10	• • Direct field-oriented control; Rotor flux feed-back control
13/08	• by sliding current collector along winding	21/12	• Stator flux based control involving the use of rotor position or rotor speed sensors
13/10	• by moving core, coil winding, or shield, e.g. by induction regulator	21/13	• Observer control, e.g. using Luenberger observers or Kalman filters
13/12	• by varying magnetic bias	21/14	• Estimation or adaptation of machine parameters, e.g. flux, current or voltage
15/00	Arrangements for controlling dynamo-electric brakes or clutches (controlling speed of dynamo-electric motors by means of a separate brake H02P 29/04 , vector control H02P 21/00 {see provisionally also H02K 49/00 and H02P 29/0022 })	21/141	• • {Flux estimation}
15/02	• Conjoint control of brakes and clutches	21/143	• • {Inertia or moment of inertia estimation}
17/00	Arrangements for controlling dynamo-electric gears (vector control H02P 21/00)	21/16	• • Estimation of constants, e.g. the rotor time constant
21/00	Arrangements or methods for the control of electric machines by vector control, e.g. by control of field orientation	21/18	• • Estimation of position or speed
NOTES		21/20	• • Estimation of torque
1. When classifying in this group, classification should also be made in group H02P 25/00 when the method of control is characterised by the kind of motor being controlled.		21/22	• Current control, e.g. using a current control loop
2. When classifying in this group, classification should also be made in group H02P 27/00 when the method of control is characterised by the kind of supply voltage of the motor being controlled.		21/24	• Vector control not involving the use of rotor position or rotor speed sensors
21/0003	• {Control strategies in general, e.g. linear type, e.g. P, PI, PID, using robust control}	21/26	• • Rotor flux based control
21/0007	• • {using sliding mode control}	21/28	• • Stator flux based control
21/001	• • {using fuzzy control}	21/30	• • • Direct torque control [DTC] or field acceleration method [FAM]
21/0014	• • {using neural networks}	21/32	• • Determining the initial rotor position (H02P 21/34 takes precedence)
21/0017	• • {Model reference adaptation, e.g. MRAS or MRAC, useful for control or parameter estimation}	21/34	• Arrangements for starting
21/0021	• • {using different modes of control depending on a parameter, e.g. the speed}	21/36	• Arrangements for braking or slowing; Four quadrant control
21/0025	• • {implementing a off line learning phase to determine and store useful data for on-line control}	21/50	• {Vector control arrangements or methods not otherwise provided for in H02P 21/00 - H02P 21/36 }
21/0085	• {specially adapted for high speeds, e.g. above nominal speed}	23/00	Arrangements or methods for the control of AC motors characterised by a control method other than vector control
21/0089	• • {using field weakening}	NOTE	
21/02	• specially adapted for optimising the efficiency at low load	When classifying in this group, subject matter also relating to groups H02P 21/00 , H02P 25/00 or H02P 27/00 is further classified in those groups whenever appropriate.	
21/04	• specially adapted for very low speeds	23/0004	• {Control strategies in general, e.g. linear type, e.g. P, PI, PID, using robust control}
		23/0009	• • {using sliding mode control}
		23/0013	• • {using fuzzy control}
		23/0018	• • {using neural networks}
		23/0022	• • {Model reference adaptation, e.g. MRAS or MRAC, useful for control or parameter estimation}
		23/0027	• • {using different modes of control depending on a parameter, e.g. the speed}
		23/0031	• • {implementing a off line learning phase to determine and store useful data for on-line control}
		23/0077	• {Characterised by the use of a particular software algorithm}
		23/0086	• {specially adapted for high speeds, e.g. above nominal speed}

- 23/009 . . {using field weakening}
- 23/02 . specially adapted for optimising the efficiency at low load
- 23/03 . specially adapted for very low speeds
- 23/04 . specially adapted for damping motor oscillations, e.g. for reducing hunting
- 23/06 . Controlling the motor in four quadrants
- 23/07 . . Polyphase or monophas asynchronous induction motors
- 23/08 . Controlling based on slip frequency, e.g. adding slip frequency and speed proportional frequency
- 23/10 . Controlling by adding a dc current (dc current braking H02P 3/24)
- 23/12 . Observer control, e.g. using Luenberger observers or Kalman filters
- 23/14 . Estimation or adaptation of motor parameters, e.g. rotor time constant, flux, speed, current or voltage
- 23/16 . Controlling the angular speed of one shaft (H02P 23/18 takes precedence)
- 23/18 . Controlling the angular speed together with angular position or phase
- 23/183 . . {of one shaft without controlling the prime mover}
- 23/186 . . {of one shaft by controlling the prime mover}
- 23/20 . Controlling the acceleration or deceleration
- 23/22 . Controlling the speed digitally using a reference oscillator, a speed proportional pulse rate feedback and a digital comparator
- 23/24 . Controlling the direction, e.g. clockwise or counterclockwise
- 23/26 . Power factor control [PFC]
- 23/28 . Controlling the motor by varying the switching frequency of switches connected to a DC supply and the motor phases
- 23/30 . Direct torque control [DTC] or field acceleration method [FAM]
- 25/00 Arrangements or methods for the control of AC motors characterised by the kind of AC motor or by structural details**
- NOTE**
When classifying in this group, subject matter also relating to groups [H02P 21/00](#), [H02P 23/00](#) or [H02P 27/00](#) is further classified in those groups whenever appropriate.
- 25/02 . characterised by the kind of motor
- 25/022 . . Synchronous motors (H02P 25/064 takes precedence)
- 25/024 . . . controlled by supply frequency
- 25/026 thereby detecting the rotor position
- 25/028 . . . with four quadrant control
- 25/03 . . . with brushless excitation
- 25/032 . . Reciprocating, oscillating or vibrating motors
- 25/034 . . . Voice coil motors (voice coil motors driven by DC power H02P 7/025)
- 25/04 . . Single phase motors, e.g. capacitor motors
- 25/06 . . Linear motors
- 25/062 . . . of the induction type
- 25/064 . . . of the synchronous type
- 25/066 of the stepping type
- 25/08 . . Reluctance motors
- 25/0805 . . . {whereby the speed is regulated by measuring the motor speed and comparing it with a given physical value}
- 25/083 . . . Arrangements for increasing the switching speed from one coil to the next one
- 25/086 . . . Commutation
- 25/089 Sensorless control (direct torque control H02P 23/30)
- 25/092 . . . Converters specially adapted for controlling reluctance motors
- 25/0925 {wherein the converter comprises only one switch per phase}
- 25/098 . . . Arrangements for reducing torque ripple
- 25/10 . . Commutator motors, e.g. repulsion motors
- 25/102 . . . {Repulsion motors}
- 25/105 . . . {Four quadrant control}
- 25/107 . . . {Polyphase or monophas commutator motors}
- 25/12 . . . with shiftable brushes
- 25/14 . . . Universal motors (H02P 25/12 takes precedence)
- 25/145 {whereby the speed is regulated by measuring the motor speed and comparing it with a given physical value, speed feedback}
- 25/16 . characterised by the circuit arrangement or by the kind of wiring
- 25/18 . . with arrangements for switching the windings, e.g. with mechanical switches or relays
- 25/182 . . . {whereby the speed is regulated by using centrifugal devices, e.g. switch, resistor}
- 25/184 . . . {wherein the motor speed is changed by switching from a delta to a star, e.g. wye, connection of its windings, or vice versa}
- 25/186 . . . {whereby the speed is regulated by using a periodic interrupter (H02P 25/30 takes precedence)}
- 25/188 . . . {wherein the motor windings are switched from series to parallel or vice versa to control speed or torque}
- 25/20 . . . for pole-changing
- 25/22 . . Multiple windings; Windings for more than three phases
- 25/24 . . Variable impedance in stator or rotor circuit
- 25/26 . . . with arrangements for controlling secondary impedance
- 25/28 . . using magnetic devices with controllable degree of saturation, e.g. transducers
- 25/30 . . the motor being controlled by a control effected upon an ac generator supplying it
- 25/32 . . using discharge tubes
- 25/325 . . . {whereby the speed is regulated by measuring the motor speed and comparing it with a given physical value}
- 27/00 Arrangements or methods for the control of AC motors characterised by the kind of supply voltage (of two or more motors H02P 5/00; of synchronous motors with electronic commutators H02P 6/00; of DC motors H02P 7/00; of stepping motors H02P 8/00)**
- NOTE**
When classifying in this group, subject matter also relating to groups [H02P 21/00](#), [H02P 23/00](#) or

H02P

H02P 27/00

(continued)

[H02P 25/00](#) is further classified in those groups whenever appropriate

- 27/02 . using supply voltage with constant frequency and variable amplitude
- 27/024 . . using AC supply for only the rotor circuit or only the stator circuit
- 27/026 . . {whereby the speed is regulated by measuring the motor speed and comparing it with a given physical value}
- 27/04 . using variable-frequency supply voltage, e.g. inverter or converter supply voltage
- 27/045 . . {whereby the speed is regulated by measuring the motor speed and comparing it with a given physical value}
- 27/047 . . {V/F converter, wherein the voltage is controlled proportionally with the frequency}
- 27/048 . . using AC supply for only the rotor circuit or only the stator circuit
- 27/05 . . using AC supply for both the rotor and the stator circuits, the frequency of supply to at least one circuit being variable
- 27/06 . . using dc to ac converters or inverters ([H02P 27/05](#) takes precedence)
- 27/08 . . . with pulse width modulation
- 27/085 {wherein the PWM mode is adapted on the running conditions of the motor, e.g. the switching frequency}
- 27/10 using bang-bang controllers
- 27/12 pulsing by guiding the flux vector, current vector or voltage vector on a circle or a closed curve, e.g. for direct torque control
- 27/14 with three or more levels of voltage
- 27/16 . . using ac to ac converters without intermediate conversion to dc ([H02P 27/05](#) takes precedence)
- 27/18 . . . varying the frequency by omitting half waves

29/00 Arrangements for regulating or controlling electric motors, appropriate for both AC and DC motors (arrangements for starting electric motors [H02P 1/00](#); arrangements for stopping or slowing electric motors [H02P 3/00](#); control of motors that can be connected to two or more different electric power supplies [H02P 4/00](#); regulating or controlling the speed or torque of two or more electric motors [H02P 5/00](#); vector control [H02P 21/00](#))

- 29/0016 . {Control of angular speed of one shaft without controlling the prime mover}
- 29/0022 . . {Controlling a brake between the prime mover and the load}
- 29/0027 . . {Controlling a clutch between the prime mover and the load}
- 29/02 . Providing protection against overload without automatic interruption of supply (protection against faults of stepper motors [H02P 8/36](#))

NOTE

Informative note

References listed below indicate places which could also be of interest when carrying out a search in respect of the subject matter covered by the preceding group:

Emergency protective circuit arrangements with automatic interruption if supply, in general [H02H 7/08](#);

Emergency protective circuit arrangements for limiting excess current or voltage without disconnection in general [H02H 7/08](#)

- 29/024 . . Detecting a fault condition, e.g. short circuit, locked rotor, open circuit or loss of load
- 29/0241 . . . {the fault being an overvoltage}
- 29/0243 . . . {the fault being a broken phase}
- 29/025 . . . {the fault being a power interruption}
- 29/026 . . . {the fault being a power fluctuation}
- 29/027 . . . {the fault being an over-current}
- 29/028 . . . the motor continuing operation despite the fault condition, e.g. eliminating, compensating for or remedying the fault
- 29/032 . . Preventing damage to the motor, e.g. setting individual current limits for different drive conditions
- 29/04 . by means of a separate brake
- 29/045 . . {whereby the speed is regulated by measuring the motor speed and comparing it with a given physical value}
- 29/10 . for preventing overspeed or under speed
- 29/20 . for controlling one motor used for different sequential operations
- 29/40 . Regulating or controlling the amount of current drawn or delivered by the motor for controlling the mechanical load
- 29/50 . Reduction of harmonics
- 29/60 . Controlling or determining the temperature of the motor or of the drive ([H02P 29/02](#) takes precedence)
- 29/62 . . for raising the temperature of the motor
- 29/64 . . Controlling or determining the temperature of the winding
- 29/66 . . Controlling or determining the temperature of the rotor
- 29/662 . . . {the rotor having permanent magnets ([H02P 29/67](#) takes precedence)}
- 29/664 . . . {the rotor having windings}
- 29/666 {by rotor current detection}
- 29/67 . . {Controlling or determining the motor temperature by back electromotive force [back-EMF] evaluation}
- 29/68 . . based on the temperature of a drive component or a semiconductor component
- 29/685 . . . {compensating for Hall sensor temperature non-linearity}

31/00 Arrangements for regulating or controlling electric motors not provided for in groups [H02P 1/00](#) - [H02P 5/00](#), [H02P 7/00](#) or [H02P 21/00](#) - [H02P 29/00](#)

Indexing scheme associated with groups relating to the arrangements for controlling electric generators

2101/00 Special adaptation of control arrangements for generators

- 2101/10 . for water-driven turbines
- 2101/15 . for wind-driven turbines
- 2101/20 . for steam-driven turbines
- 2101/25 . for combustion engines
- 2101/30 . for aircraft
- 2101/35 . for ships
- 2101/40 . for railway vehicles

2101/45	• for motor vehicles, e.g. car alternators	2205/03	• Power loop, i.e. comparison of the motor power with a power reference
2103/00	Controlling arrangements characterised by the type of generator	2205/05	• Torque loop, i.e. comparison of the motor torque with a torque reference
2103/10	• of the asynchronous type	2205/07	• Speed loop, i.e. comparison of the motor speed with a speed reference
2103/20	• of the synchronous type		
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2201/00	Indexing scheme relating to controlling arrangements characterised by the converter used	2207/00	Indexing scheme relating to controlling arrangements characterised by the type of motor
2201/01	• AC-AC converter stage controlled to provide a defined AC voltage	2207/01	• Asynchronous machines
2201/03	• AC-DC converter stage controlled to provide a defined DC link voltage (general aspects of plural converters in cascade H02M)	2207/03	• Double rotor motors or generators, i.e. electromagnetic transmissions having double rotor with motor and generator functions, e.g. for electrical variable transmission
2201/05	• Capacitive half bridge, i.e. resonant inverter having two capacitors and two switches	2207/05	• Synchronous machines, e.g. with permanent magnets or DC excitation
2201/07	• DC-DC step-up or step-down converter inserted between the power supply and the inverter supplying the motor, e.g. to control voltage source fluctuations, to vary the motor speed (general aspects of plural converters in cascade H02M)	2207/055	• • Surface mounted magnet motors
2201/09	• Boost converter, i.e. DC-DC step up converter increasing the voltage between the supply and the inverter driving the motor (general aspects of plural converters in cascade H02M)	2207/07	• Doubly fed machines receiving two supplies both on the stator only wherein the power supply is fed to different sets of stator windings or to rotor and stator windings
2201/11	• Buck converter, i.e. DC-DC step down converter decreasing the voltage between the supply and the inverter driving the motor (general aspects of plural converters in cascade H02M)	2207/073	• • wherein only one converter is used, the other windings being supplied without converter, e.g. doubly-fed induction machines
2201/13	• DC-link of current link type, e.g. typically for thyristor bridges, having an inductor in series with rectifier	2207/076	• • wherein both supplies are made via converters: especially doubly-fed induction machines; e.g. for starting
2201/15	• Power factor Correction [PFC] circuit generating the DC link voltage for motor driving inverter (motor power factor control H02P 23/26)		
2203/00	Indexing scheme relating to controlling arrangements characterised by the means for detecting the position of the rotor	2209/00	Indexing scheme relating to controlling arrangements characterised by the waveform of the supplied voltage or current
2203/01	• Motor rotor position determination based on the detected or calculated phase inductance, e.g. for a Switched Reluctance Motor	2209/01	• Motors with neutral point connected to the power supply
2203/03	• Determination of the rotor position, e.g. initial rotor position, during standstill or low speed operation	2209/03	• Motors with neutral point disassociated, i.e. the windings ends are not connected directly to a common point
2203/05	• Determination of the rotor position by using two different methods and/or motor models	2209/05	• Polyphase motors supplied from a single-phase power supply or a DC power supply
2203/07	• Motor variable determination based on the ON-resistance of a power switch, i.e. the voltage across the switch is measured during the ON state of the switch and used to determine the current in the motor and to calculate the speed	2209/07	• Trapezoidal waveform
2203/09	• Motor speed determination based on the current and/or voltage without using a tachogenerator or a physical encoder	2209/09	• PWM with fixed limited number of pulses per period
2203/11	• Determination or estimation of the rotor position or other motor parameters based on the analysis of high frequency signals (position detection of motors with electronic commutators in dependence of the position H02P 6/185)	2209/095	• • One pulse per half period
		2209/11	• Sinusoidal waveform
2205/00	Indexing scheme relating to controlling arrangements characterised by the control loops	2209/13	• Different type of waveforms depending on the mode of operation
2205/01	• Current loop, i.e. comparison of the motor current with a current reference		